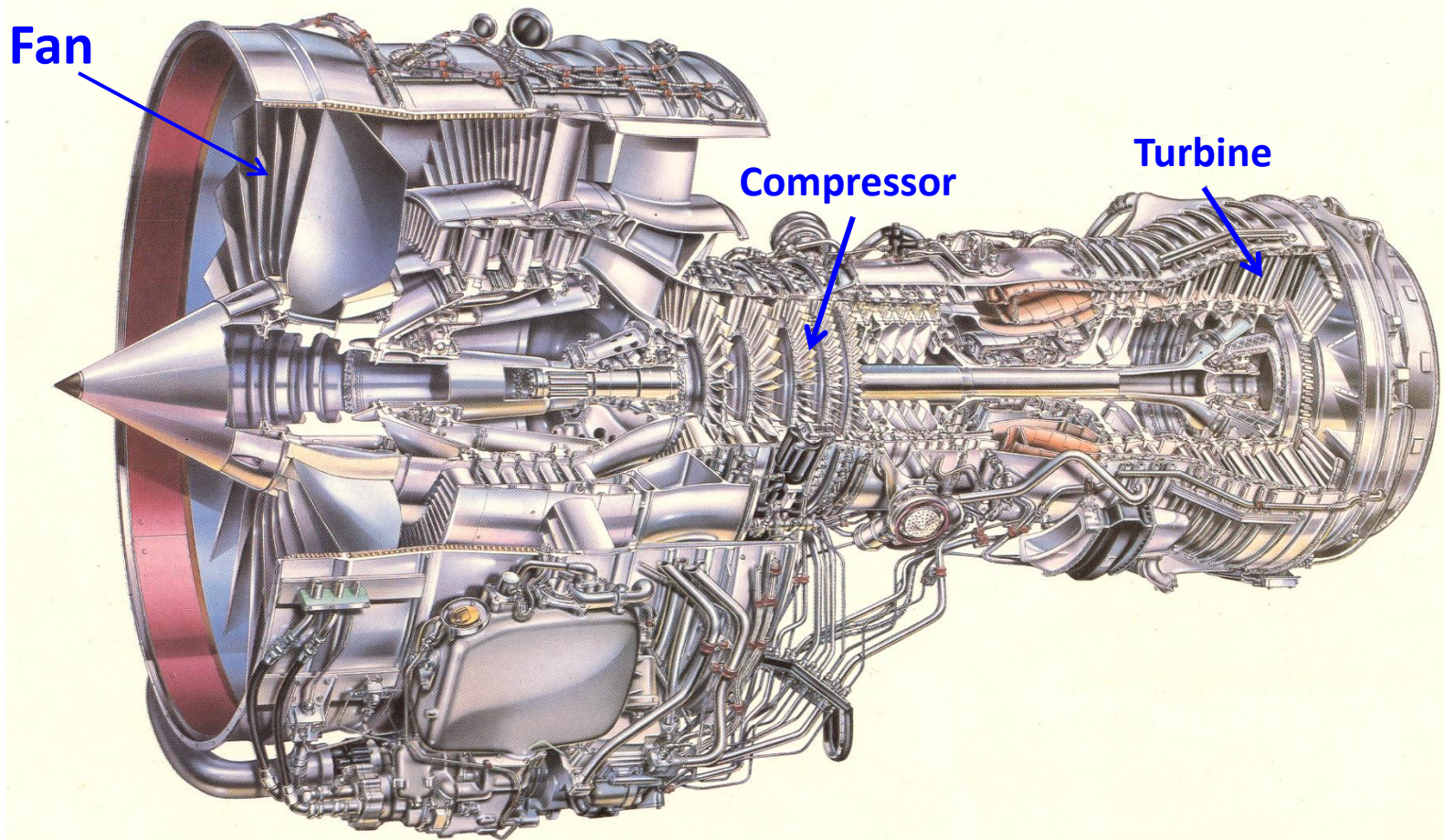
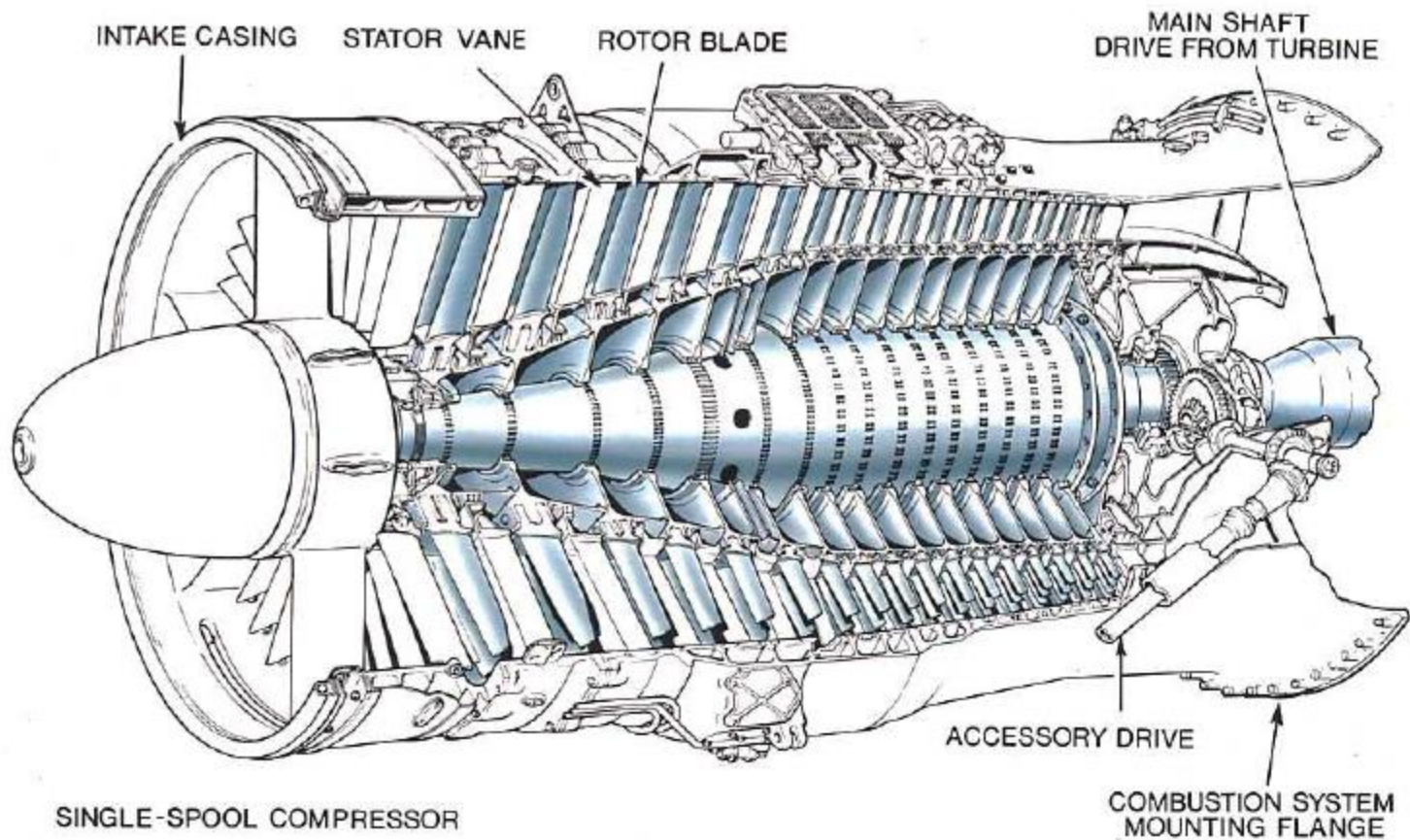


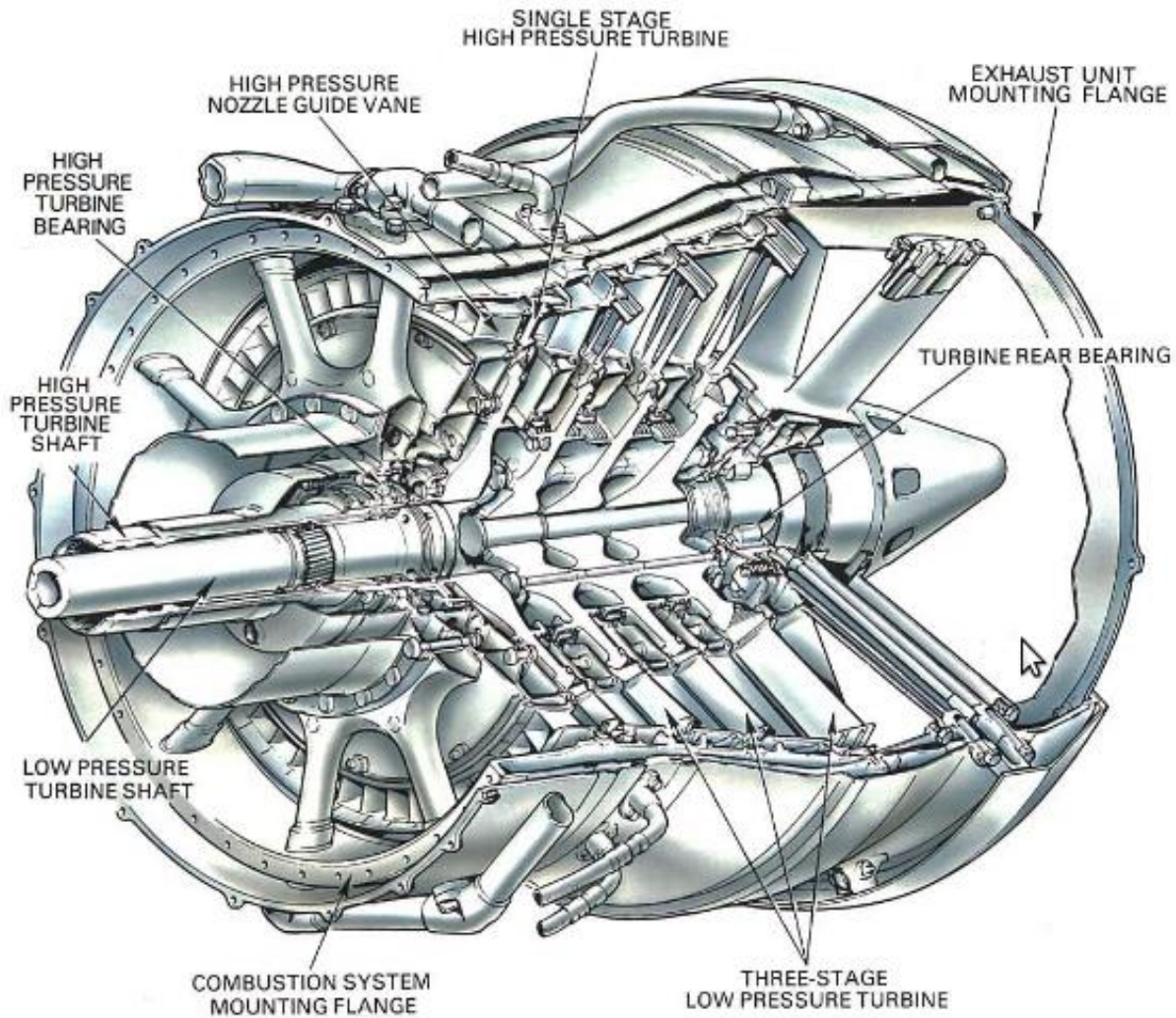
- Recap: Lecture 1: 21st July 2015, 1530-hrs.
 - Introduction
 - Aims of the course
 - Course contents
 - Text books/references
 - Evaluation scheme and course schedule



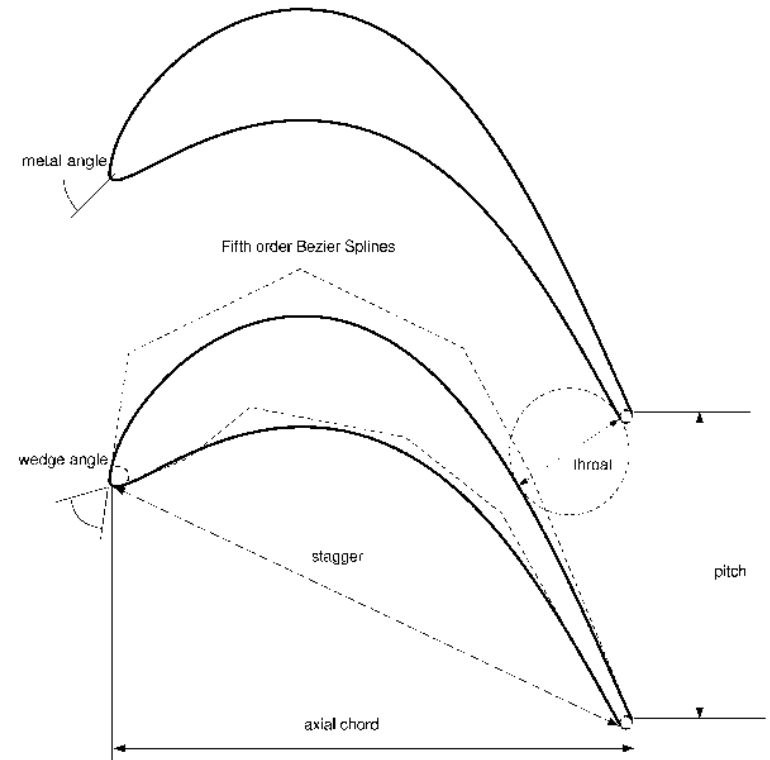
A modern high bypass turbofan engine



Typical multi-stage axial flow compressor



A twin turbine and shaft system



Turbine nozzle and rotor blade geometries

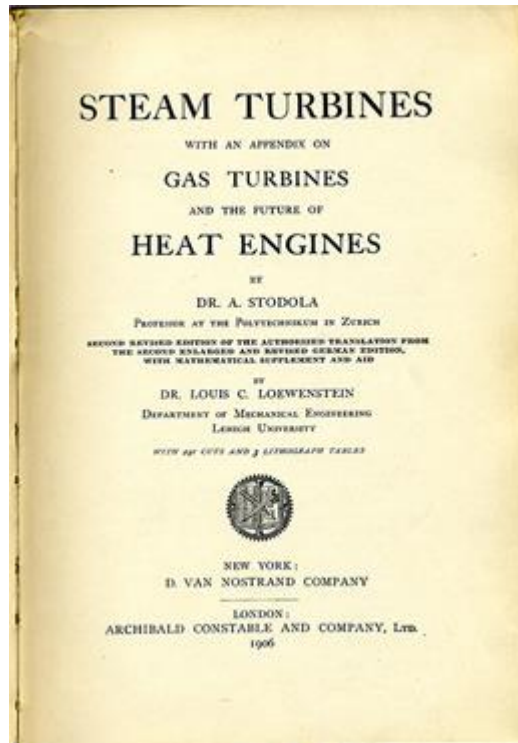


Source: Mitsubishi Heavy Industries, Ltd.

Centrifugal compressor

	787 Engines: GENx-1B Trent 1000	767 Engines: GE CF6-80C2 RR RB211-524G/H
Bypass Ratio	~10	~5
Overall Pressure Ratio	~50	~33
Thrust Class	53,000–74,000 lbf	53,000–63,000 lbf
Fan Diameter	111–112 in	86–93 in
Specific Fuel Consumption	15% lower	Base
Noise	ICAO Chapter 4	ICAO Chapter 3
Emissions	CAEP/8 (2014)	CAEP/2

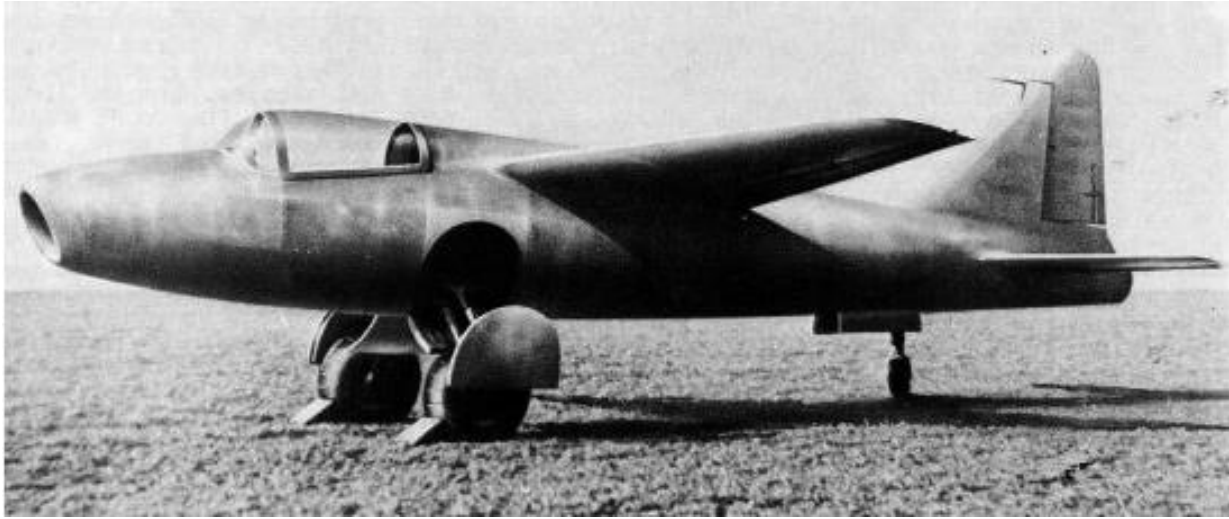
Source: http://www.boeing.com/commercial/aeromagazine/articles/2012_q3/2/



Commissioning of world's first industrial gas turbine, Neuchatel, 1939 (Stodola at age 80)



Frank Whittle and Hans von Ohain



First turbojet-powered aircraft – Ohain's engine on He 178 (1939)

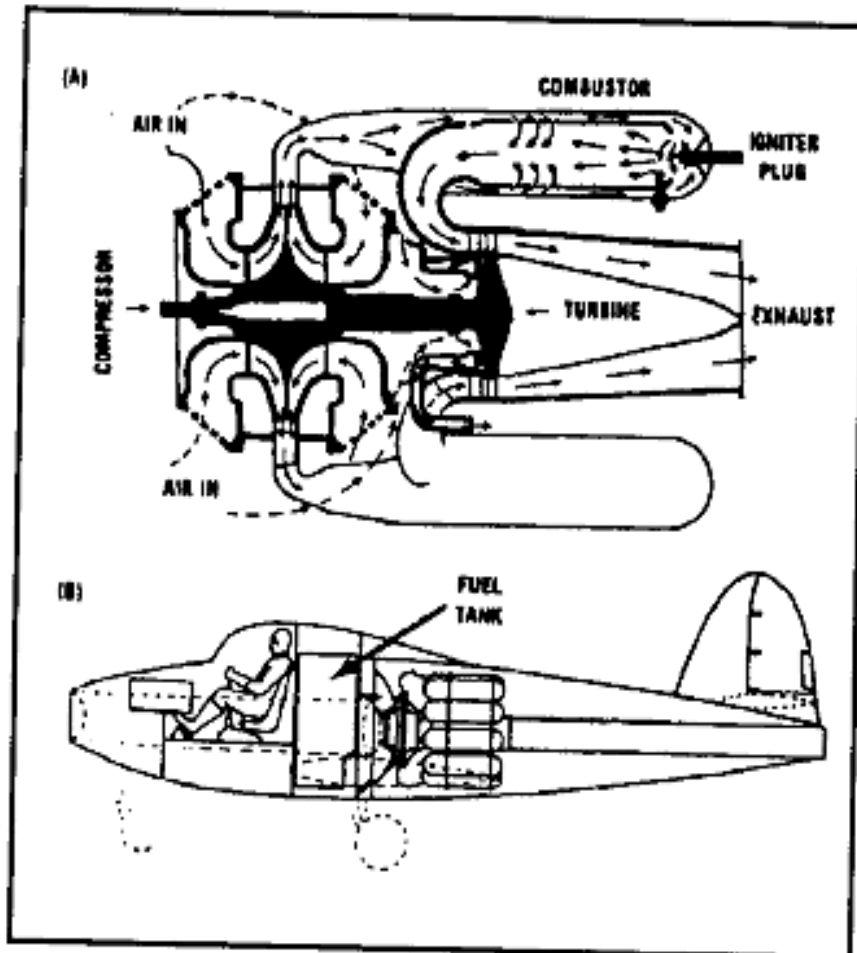
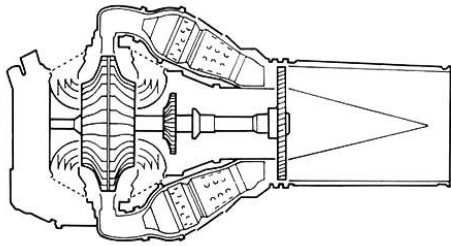


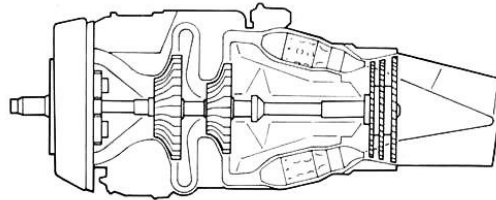
Figure 2-5. A – Whittle's Reverse-Flow Combustion Chamber. B – Fuselage Arrangement of the E28/39 Experimental



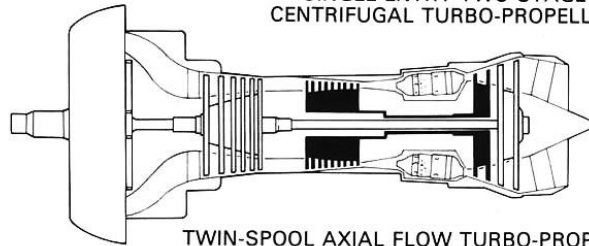
Powered the Gloster E28/39 Britain on 15 May 1941.



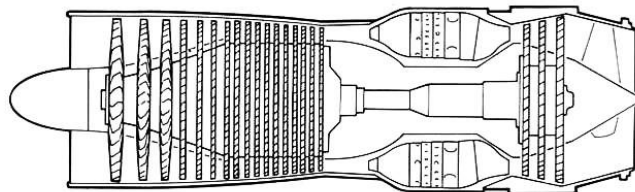
DOUBLE-ENTRY SINGLE-STAGE
CENTRIFUGAL TURBO-JET



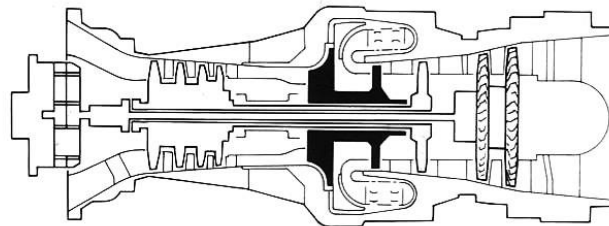
SINGLE-ENTRY TWO-STAGE
CENTRIFUGAL TURBO-PROPELLER



TWIN-SPOOL AXIAL FLOW TURBO-PROPELLER

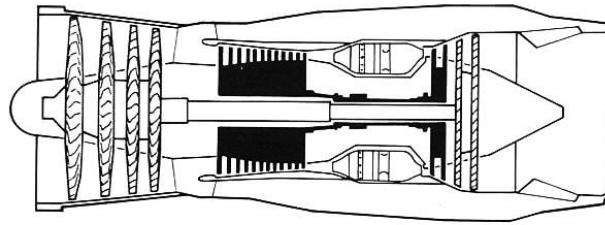


SINGLE-SPOOL AXIAL FLOW TURBO-JET

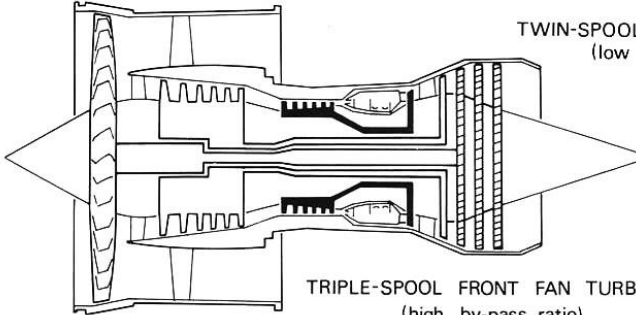


TWIN-SPOOL TURBO-SHAFT (with free-power turbine)

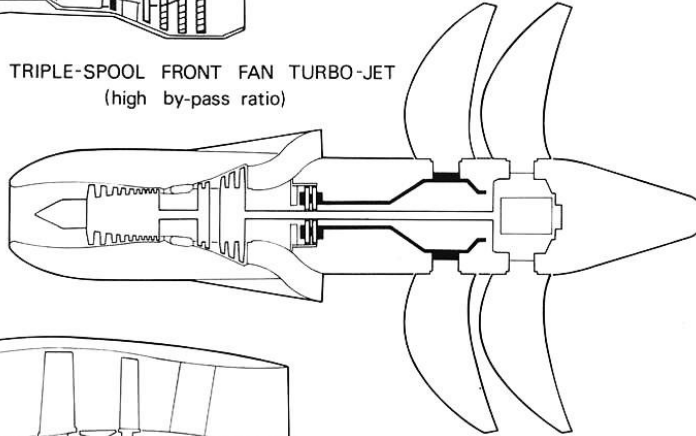
Types of Gas Turbine Engines



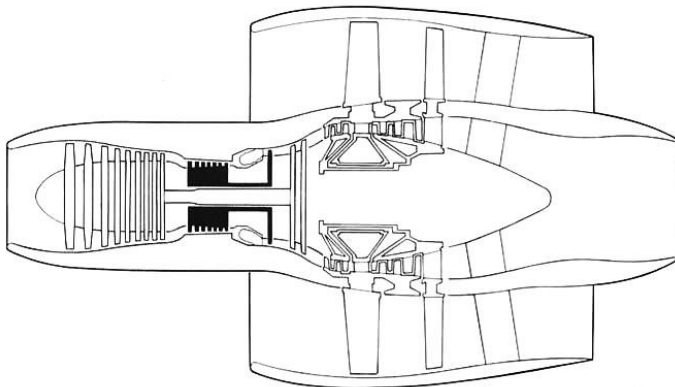
TWIN-SPOOL BY-PASS TURBO-JET
(low by-pass ratio)



TRIPLE-SPOOL FRONT FAN TURBO-JET
(high by-pass ratio)



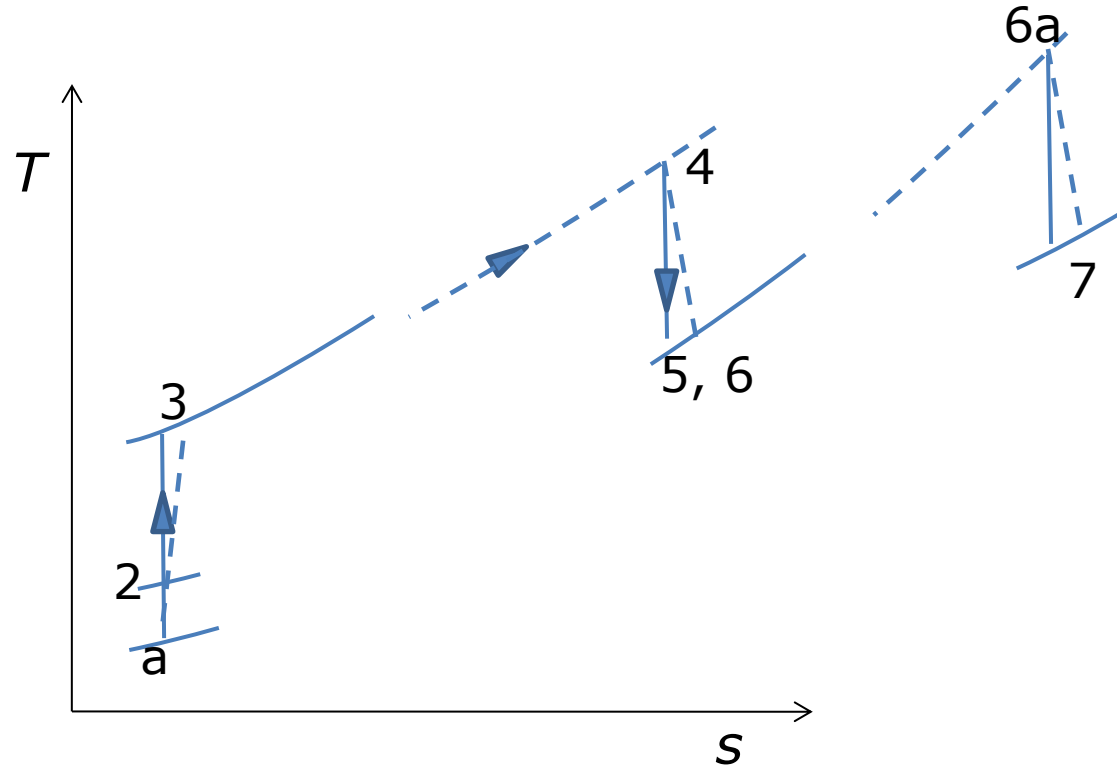
PROP-FAN - CONCEPT



CONTRA-ROTATING FAN - CONCEPT (high by-pass ratio)

Types of Gas Turbine Engines

Real cycle for turbojet engines



Real turbojet cycle (with afterburning) on a T-s diagram

Review of Thermodynamic Concepts

Total energy of a system

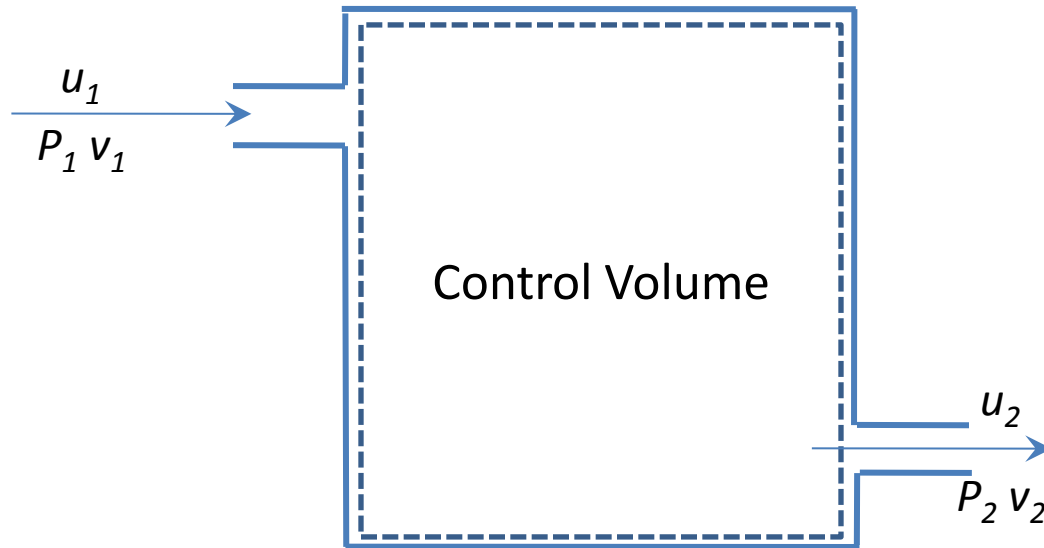
- In the absence of magnetic, electric, and surface tension effects, the total energy of a system consists of the kinetic, potential, and internal energies

$$E = U + KE + PE = U + \frac{mV^2}{2} + mgz \quad (\text{kJ})$$

or, on a unit mass basis

$$e = u + ke + pe = u + \frac{V^2}{2} + gz \quad (\text{kJ/kg})$$

Enthalpy



The combination $u + Pv$ is frequently encountered in the analysis of control volumes

Enthalpy

- The combination of internal energy u and Pv is often encountered in the analysis of control volumes
- Enthalpy is a combination property

$$\text{Enthalpy, } h = u + Pv \text{ (kJ/kg)}$$

$$H = U + PV \text{ (kJ)}$$

- Enthalpy is also often referred to as heat content
- Process in which enthalpy is constant:
isenthalpic process

Entropy

- Entropy is an extensive property of a system and sometimes is referred to as **total entropy**. Entropy per unit mass, designated s , is an intensive property and has the unit kJ/kg.K
- The entropy change of a system during a process can be determined by

$$\Delta S = S_2 - S_1 = \int_1^2 \left(\frac{\delta Q}{T} \right)_{\text{int. rev.}} \quad (\text{kJ/kg})$$

Entropy

- Entropy is a property, and like all other properties, it has fixed values at fixed states.
- Therefore, the entropy change dS between two specified states is the same no matter what path, reversible or irreversible.

Temperature-entropy plot

$$dS = \frac{dQ_{rev}}{T}$$

If the process is reversible and adiabatic, $dQ_{rev} = 0$

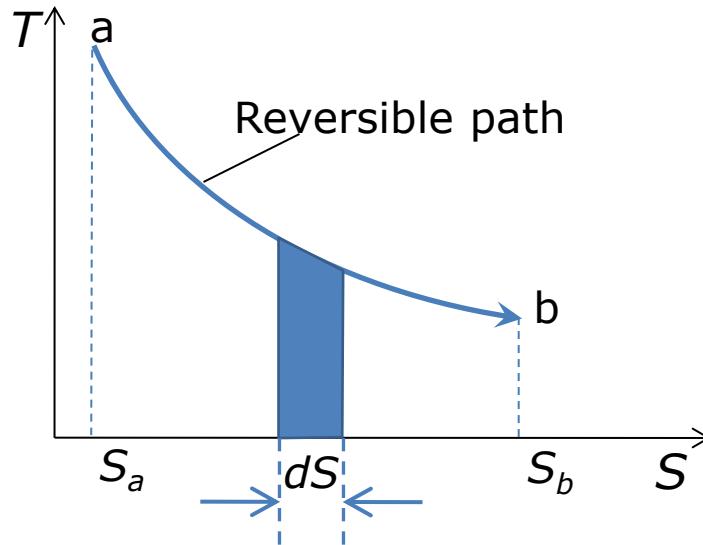
$\therefore dS = 0$ or $S = \text{constant}$

- A reversible adiabatic process is, therefore, and **isentropic process**.

$$dQ_{rev} = TdS$$

$$\text{or, } Q_{rev} = \int TdS$$

Temperature-entropy plot



$$Q_{rev} = \int_a^b T dS = T(S_b - S_a)$$

- The area under the reversible path on the T-S plot represents heat transfer during that process.

Isentropic processes

- A process where, $\Delta s=0$
- An isentropic process can serve as an appropriate model for actual processes.
- Isentropic processes enable us to define efficiencies for processes to compare the actual performance of these devices to the performance under idealized conditions.
- A reversible adiabatic process is necessarily isentropic, but an isentropic process is not necessarily a reversible adiabatic process.

TdS equations

- From the first law for an internally reversible process, we know that

$$dQ_{\text{int rev}} - dW_{\text{int rev, out}} = dU$$

Since, $dQ_{\text{int rev}} = TdS$ and $dW_{\text{int rev, out}} = PdV$

$$TdS = dU + PdV \text{ or, } Tds = du + Pdv$$

- This is known as the **first TdS equation**.

TdS equations

- From the definition of enthalpy, we know that,

$$h = u + Pv$$

$$\text{or, } dh = du + Pdv + vdP$$

$$\text{since, } Tds = du + Pdv,$$

$$Tds = dh - vdP$$

- This is known as the **second TdS equation**.

Entropy change of ideal gases

- For ideal gases we know that,

$$du = c_v dT, P = RT / v$$

From the TdS relations,

$$ds = c_v \frac{dT}{T} + R \frac{dv}{v}$$

- The entropy change for a process,

$$s_2 - s_1 = \int_1^2 c_v(T) \frac{dT}{T} + R \ln \frac{v_2}{v_1}$$

Entropy change of ideal gases

If we use these relations,

$$dh = c_p dT, \quad v = RT / P$$

Then, from the TdS relations,

$$s_2 - s_1 = \int_1^2 c_p(T) \frac{dT}{T} - R \ln \frac{P_2}{P_1}$$

- Usually, we assume average values of c_p and c_v in the above equations and thus can replace $c_p(T)$ with $c_{p,av}$ and $c_v(T)$ with $c_{v,av}$.

Energy analysis of steady flow systems

- For single entry and exit devices,

$$\dot{Q} - \dot{W} = \dot{m} \left[h_2 - h_1 + \frac{V_2^2 - V_1^2}{2} + g(z_2 - z_1) \right]$$

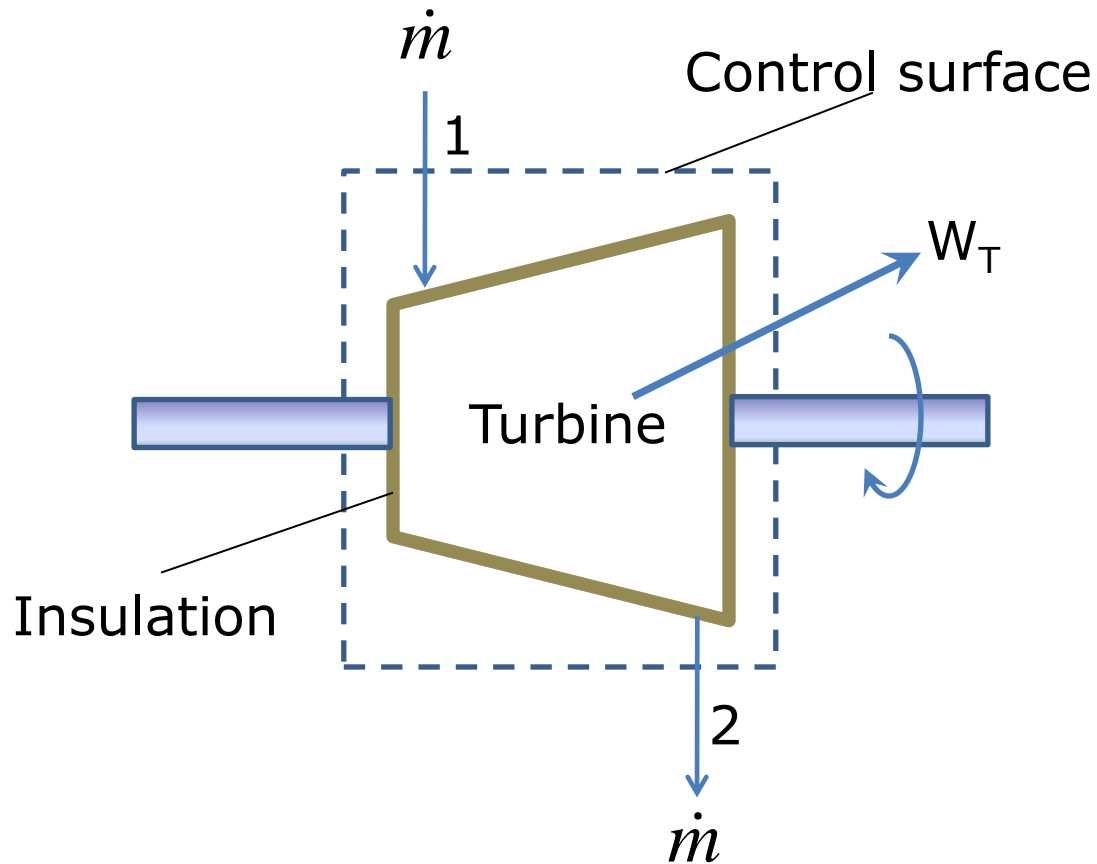
or per unit mass,

$$\dot{q} - \dot{w} = h_2 - h_1 + \frac{V_2^2 - V_1^2}{2} + g(z_2 - z_1)$$

Turbines and compressors

- Pumps, compressors and fans: used to increase the pressure of a fluid and require work input.
- Turbines generate work.
- Q , KE and PE may or may not be zero.
- Usually PE is negligibly small.

Turbines and compressors



Turbines and compressors

- For a turbine for eg., the energy equation would be:

$$\dot{m}\left(h_1 + \frac{V_1^2}{2} + gz_1\right) = \dot{W}_{out} + \dot{m}\left(h_2 + \frac{V_2^2}{2} + gz_2\right)$$

If KE and PE are negligible,

$$\dot{W}_{out} = \dot{m}(h_1 - h_2)$$

Stagnation properties

- Enthalpy represents the total energy of a fluid in the absence of potential and kinetic energies.
- For high speed flows, though potential energy may be negligible, but not kinetic energy.
- Combination of enthalpy and KE is called **stagnation enthalpy** (or total enthalpy)

$$h_0 = h + V^2/2 \quad (\text{kJ/kg})$$

Stagnation enthalpy Static enthalpy Kinetic energy

Stagnation properties

- Consider a steady flow through a duct (no shaft work, heat transfer etc.).
- The steady flow energy equation for this

is:
$$h_1 + V_1^2/2 = h_2 + V_2^2/2$$

or,
$$h_{01} = h_{02}$$

- That is in the absence of any heat and work interactions, the stagnation enthalpy remains a constant during a steady flow process.

Stagnation properties

- If the fluid were brought to rest at state 2,

$$h_1 + V_1^2/2 = h_2 = h_{02}$$

- The stagnation enthalpy represents the enthalpy of a fluid when it is brought to rest adiabatically.
- During a stagnation process, the kinetic energy of a fluid is converted to enthalpy (internal energy + flow energy), which results in an increase in the fluid temperature and pressure.

Stagnation properties

- When the fluid is approximated as an ideal gas with constant specific heats,

$$c_p T_0 = c_p T + V^2/2$$

$$\text{or, } T_0 = T + V^2/2c_p$$

- T_0 is called the **stagnation temperature** and represents the temperature an ideal gas attains when it is brought to rest adiabatically.
- The term $V^2/2c_p$ corresponds to the temperature rise during such a process and is called the **dynamic temperature**.

Stagnation properties

- The pressure a fluid attains when brought to rest isentropically is called the **stagnation pressure, P_0** .
- For ideal gases, from isentropic relations,

$$\frac{P_0}{P} = \left(\frac{T_0}{T} \right)^{\gamma/(\gamma-1)}$$

Similarly, for density we have,

$$\frac{\rho_0}{\rho} = \left(\frac{T_0}{T} \right)^{1/(\gamma-1)}$$